

Design of domes.

- o The roof and floor of a circular tank may be designed as a dome.
- o A dome is a type of shell obtained by the revolution of a regular curve like parabolic, circular or elliptical curve about one of its axis.
- o A dome is economical as compared to a slab as it carries the load through membrane action resulting in negligible bending moment and

Shear forces.

o A dome may be analysed by assuming it to consist of a no. of horizontal rings placed one over the other, with gradually reducing diameters towards top.

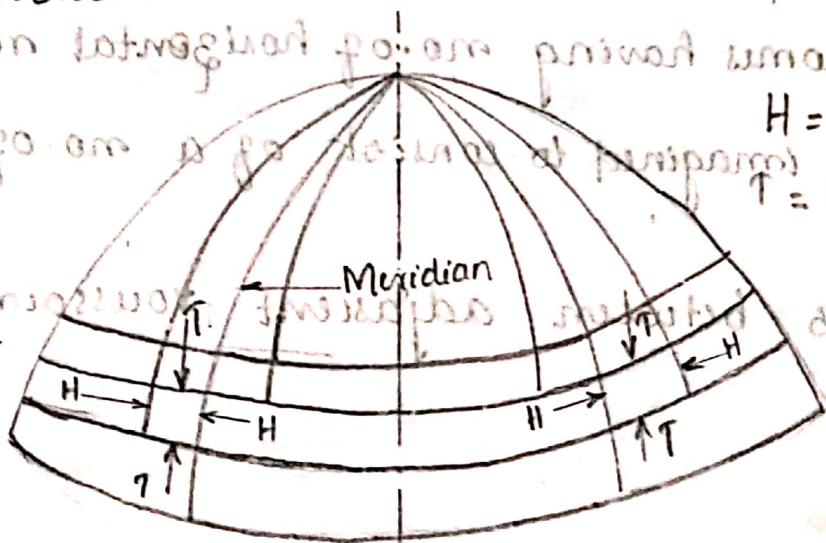
o The equilibrium of each ring is considered as independent of rings placed above it.

o Any section of the ring is subjected to following type of forces

1. Hoop or circumferential tension or compression

2. Meridional thrust.

o The hoop tension or compression acts along the circumference of the dome and the meridional thrust acts along the meridian direction.



H = hoop compression

T = Meridional thrust/
compression

Spherical dome

Meridional thrust.

- In a dome, the successive horizontal rings subtend equal angle at the center of the sphere.
- The joints between successive horizontal rings is radial.
- Every horizontal ring supports the load of the rings above it, and transmits it to the one below it.
- The reaction between the rings is tangential to the curved surface, giving rise to compression along the meridian.
- This compressive stress is called meridional thrust or meridional compression.

Hoop or circumferential tension/compression.

- In the domes having no. of horizontal rings, which may be imagined to consist of a no. of voussoirs.
- The joints between adjacent voussoirs ^{of a ring} ~~occurring~~ are radial.
- The tendency of separation of any voussoirs

will be prevented because of its wedge shape, and therefore hoop compression will be caused in each ring (θ value less than $51^\circ 49'$)

For spherical domes,

$$\text{meridional thrust } T = \frac{wR}{1 + \cos\theta} + \frac{W}{2\pi R \sin^2\theta}$$

$$\text{Hoop stress, } f = \frac{wR}{t} \left[\cos\theta - \frac{1}{1 + \cos\theta} \right] - \frac{W}{2\pi R t \sin^2\theta}$$

R = radius of the dome.

w = uniformly distributed load acting on the dome.

W = point load (any specific dead load) acting on the dome.

θ = vertical angle at the section measured from vertical axis of the dome.

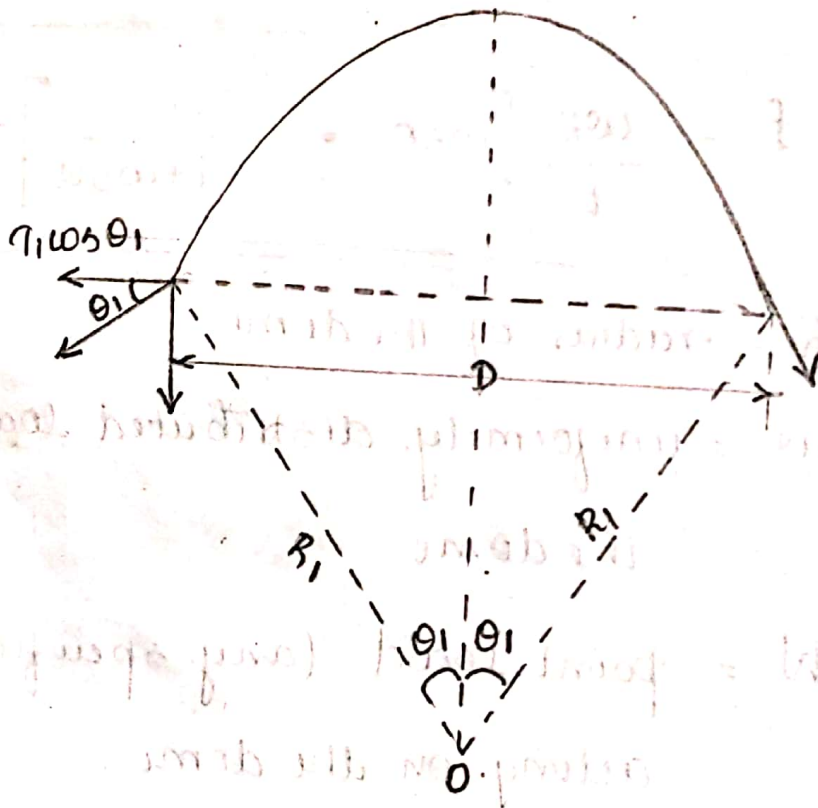
The value of hoop compression can be found by following equation.

The θ value more than $51^\circ 49'$, hoop tension will develop and for θ less than $51^\circ 49'$, hoop compression

will develop.

Ring beam

- o The ring beam subjected to hoop tension caused due to the horizontal component of the meridional thrust developed at the base of the dome.



- o Hoop tension or compression on the ring beam = $T_1 \times \cos \theta \times \frac{D}{2}$ (T_r)

where, D = Diameter of the dome.

$$T_1 = \frac{\omega R_1}{1 + \cos \theta_1} + \frac{W}{2\pi R_1 \sin^2 \theta_1}$$

The area of steel required to take this hoop tension is calculated as $\frac{T_R}{\sigma_{st}}$

The area of ring beam required to take this hoop tension is calculated by limiting the hoop stress developed to be within permissible limit.

$$\therefore \frac{T_R}{A + (m-1)A_{st}} \leq \sigma_{ct}$$

where,

A = Area of the ring beam

m = modular ratio

A_{st} = Area of steel provided in ring beam

σ_{ct} = permissible direct tensile stress in concrete.

7 Design. A spherical dome of a water tank of span 6m has a rise of 1.2m. It carries all inclusive distributed loads of 6000 N/m^2 and a lantern load of 8000 N at the crown. Design the dome. Use M20 concrete and Fe415 steel.

Given data,

$$w = 6000 \text{ N/m}^2$$

$$W = 8000 \text{ N}$$

(wt of lantern)

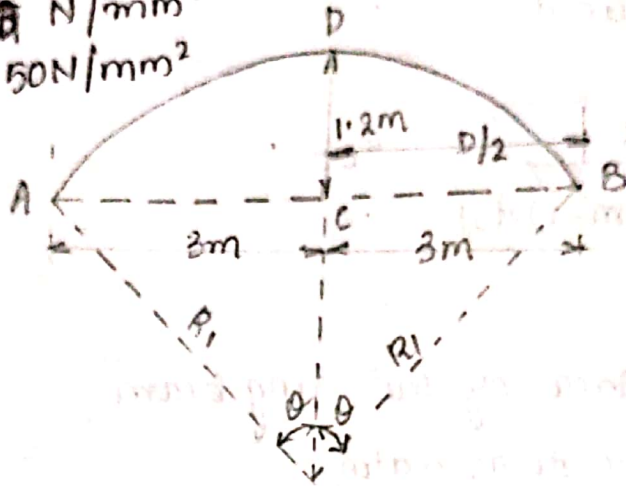
Span = 6 m.

Rise = 1.2 m.

Grade of concrete = M20

Grade of steel = Fe415

$$\left\{ \begin{array}{l} \sigma_{ct} = 1.8 \text{ N/mm}^2 \\ \sigma_{st} = 150 \text{ N/mm}^2 \end{array} \right.$$



133370
part (ii)
page 7

Let us use the property of circle

$$(2R_1 - CD) CD = \left(\frac{D}{2}\right) \left(\frac{D}{2}\right)$$
$$\left(\frac{D}{2}\right)^2$$

Find the value of radius of dome by using the property of circle

$$(2R_1 - 1.2) 1.2 = 3^2$$

$$2R_1 - 1.2 = 7.5$$

$$2R_1 = 8.7$$

$$R_1 = \underline{\underline{4.35 \text{ m}}}$$

$$\sin \theta = \frac{3}{R_1}$$

$$\theta = \sin^{-1} \left(\frac{3}{4.35} \right)$$

$$\theta = \underline{\underline{43^\circ 36'}}$$

$$\sin \theta = 0.6896$$

$$\cos \theta = 0.724$$

Meridional thrust per m run at springing level

$$T = \frac{wR}{1 + \cos \theta} + \frac{W}{2\pi R \sin^2 \theta}$$

$$= \frac{6000 \times 4.35}{1 + 0.724} + \frac{8000}{2\pi \times 4.35 \times (0.6896)^2}$$

$$T = \underline{\underline{15753.49 \text{ N}}}$$

Let us assume the thickness of dome is 100 mm

Compressive stress due to meridional thrust = $\frac{\text{load}}{\text{area}}$

$$= \frac{15753.49}{1000 \times 100}$$

$$= \underline{\underline{0.157 \text{ N/mm}^2}}$$

$$\text{Hoop stress (f)} = \frac{wR}{t} \left[\cos \theta - \frac{1}{1 + \cos \theta} \right] - \frac{W}{2\pi R t \sin^2 \theta}$$

$$= \frac{6000 \times 4.35}{100 \times 10^3} \left[0.724 - \frac{1}{1 + 0.724} \right] - \frac{8000}{2\pi \times 4.35 \times 100 \times 10^3 \times (0.6896)^2}$$

$$= \underline{\underline{31416.91274 \text{ N/m}^2}}$$

$$= \underline{\underline{0.314 \text{ N/mm}^2}}$$

As per IS 456 page no: 81, table 21

the permissible direct compressive stress for M20 concrete is
 $\underline{\underline{5 \text{ N/mm}^2}}$.

the hoop stress and stress due to meridional thrust are very low. Hence a minimum of 0.3% steel will be provided in each principle direction.

$$\begin{aligned} \text{Minimum steel requirement} &= \frac{0.3}{100} \times 10000 \times 100 \quad (b \times d) \\ &= \underline{\underline{300 \text{ mm}^2}} \end{aligned}$$

$$\begin{aligned} \text{Spacing of } 10 \text{ mm } \phi \text{ bars} &= \frac{\frac{\pi}{4} \times (10)^2 \times 1000}{300} \\ &= \underline{\underline{261.799 \text{ mm}^2}} \\ &\approx \underline{\underline{260 \text{ mm}}} \end{aligned}$$

Ring beam.

Horizontal component of meridional thrust = $\pi \cdot \cos \theta$.

$$= 15753.49 \times 0.724$$

$$= \underline{\underline{11405.526 \text{ N}}}.$$

Hoop tension in the ring beam = $T_{\text{os}} \times D/2$
 (TR)

$$= 11405.526 \times 4.3$$

$$= \underline{\underline{34216.58 \text{ N}}}$$

Safe stress in steel = 150 N/mm^2
 σ_{st}

$$A_{st} = \frac{T_R}{\sigma_{st}} = \frac{34216.58}{150} = \underline{\underline{228.11 \text{ mm}^2}}$$

Provide 4 bars of 12mm diameter.

$$A_{st \text{ pro}} = \frac{4 \times \pi \times 12^2}{4} = \underline{\underline{452.389 \text{ mm}^2}}$$

$$\frac{T_R}{A + (m-1)A_{st}} \leq \sigma_{ct}$$

$$m = \frac{280}{3 \sigma_{cbc}} = \frac{280}{3 \times 66} = \underline{\underline{1.4}}$$

$$\frac{34216.58}{A + (1.4-1)452.389} \leq 1.2$$

$$A + (1.4-1)452.389$$

$$34216.58 = 1.2A + 7057.2684$$

$$A = \underline{\underline{22632.75 \text{ mm}^2}}$$

Assume width of the beam = 250mm

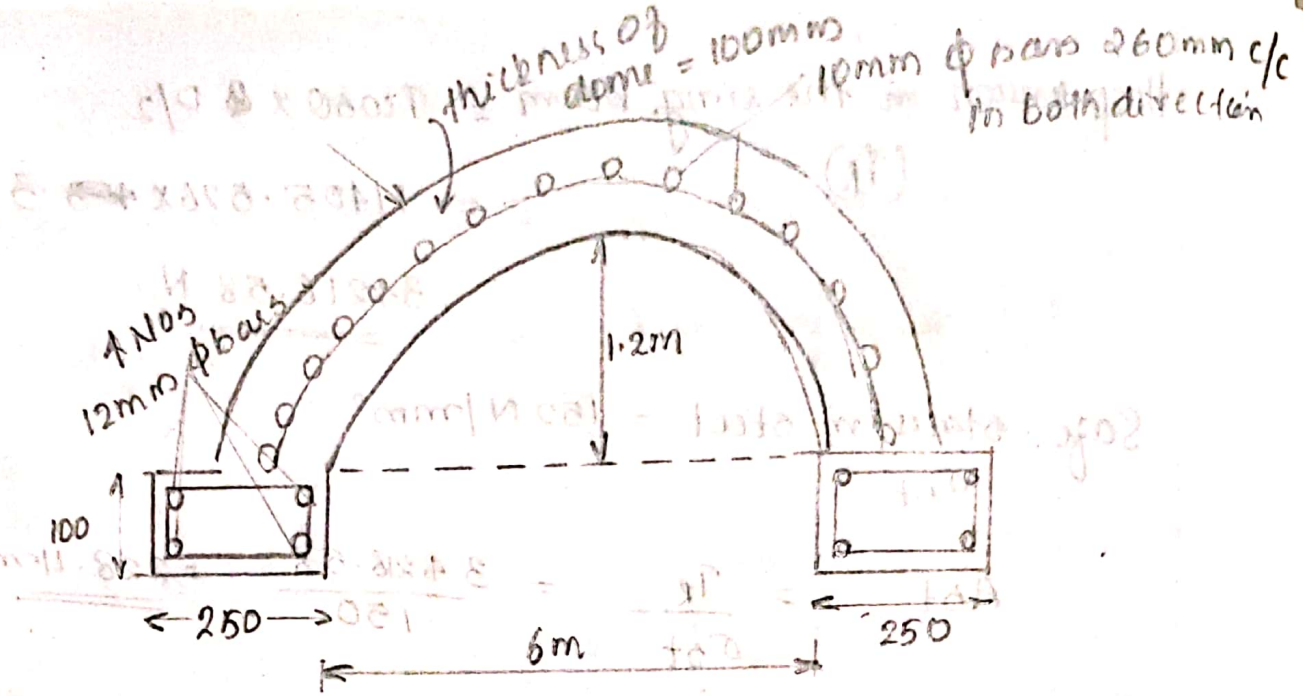
$$\text{Depth of beam} = \frac{22632.75}{250} = \underline{\underline{90.53 \text{ mm}}}$$

$$\approx \underline{\underline{100 \text{ mm}}}$$

$$\therefore D = 11.98 \times 11.311$$

Cross section of ring beam 250x100mm

$$\left(\frac{D}{2}\right)_{\text{RING}} = \dots$$



8 Design a spherical dome for a circular water tank of 500 kl capacity. The tank is supported on a masonry tower. The depth of water in tank is 5m.

Rise of the dome is 2m. Take live load on the dome as 1 kN/m^2

⇒ Given,

$$\frac{\pi}{4} \times D^2 \times \text{depth of water} = \text{capacity}$$

$$\text{capacity of tank} = 500 \text{ kL} = 500 \text{ m}^3$$

$$H = 5 \text{ m}$$

$$\frac{\pi}{4} \times D^2 \times H = 500$$

$$\frac{\pi}{4} \times D^2 \times 5 = 500$$

$$\therefore D = 11.28 \approx \underline{\underline{11.3 \text{ m}}}$$

By using the property of circle.

$$(2R_1 - \text{rise}) \text{rise} = \left(\frac{D}{2}\right)^2$$

$$(2R_1 - 2)^2 = \left(\frac{11.3}{2}\right)^2$$

$$(2R_1 - 2)^2 = 31.92$$

$$2R_1 - 2 = 5.96$$

$$\therefore R_1 = 8.98 \text{ m}$$

$$\sin \theta = \frac{11.3/2}{8.98}$$

$$\therefore \theta = \sin^{-1} \left[\frac{11.3/2}{8.98} \right]$$

$$= 38^\circ 59'$$

Assume max hoop stress will be at the top of dome where $\theta = 38^\circ 59' < 51^\circ 49'$ so hoop compression will be occur.

$$\sin \theta = 0.6295$$

$$\cos \theta = 0.777$$

meridional thrust per 'm' run at springing wall

$$T = \frac{wR \cos \theta}{1 + \cos \theta}$$

$$= \frac{1000 \times 8.98 \times 0.777}{1 + 0.777}$$

$$= 5053.46 \text{ N}$$

$$= 5053.46 \text{ N}$$

Let us assume the thickness of dome is 100 mm
 comp. stress due to meridional thrust = $\frac{\text{Load}}{\text{Area}}$

$$= \frac{5053.46}{1000 \times 100}$$

$$= 0.0505 \text{ N/mm}^2$$

$$= 0.0505 \text{ N/mm}^2$$

$$\begin{aligned} \text{Hoop stress} &= \frac{WR}{t} \left[\cos \theta - \frac{1}{1 + \cos \theta} \right] \\ &= \frac{1000 \times 9.98}{100 \times 10^3} \left[0.777 - \frac{1}{1 + 0.777} \right] \\ &= 19263.63 \text{ N/m}^2 \\ &= 0.0192 \text{ N/mm}^2 \end{aligned}$$

As per IS 456 Pg no 81 table 21.

Assume M20 concrete and Fe 415 steel.

The permissible direct compressive stress for concrete is 5 N/mm^2 .

min steel requirement $= \frac{0.3}{100} \times 1000 \times 100$

$$= 300 \text{ mm}^2$$

Spacing of 10mm ϕ bars $= \frac{\pi}{4} (10^2) \times 1000$

$$= \frac{300}{\frac{\pi}{4} (10^2) \times 1000} \times 1000$$

$$= 267.79 \text{ mm}$$

$$\approx 260 \text{ mm}$$

→ Ring Beam

Horizontal component of meridional thrust

$$\begin{aligned} &= T \cos \theta \\ &= 5053.46 \times 0.777 \\ &= 3926.53 \text{ N} \end{aligned}$$

Hoop tension in the ring beam

$$= T \cos \theta \times D/2.$$

$$= 3926.53 \times 0.777 \times \frac{11.3}{2}$$

$$= \underline{17244.014 N.}$$

safe stress in steel = 150 N/mm².

$$A_{st} = \frac{T}{\sigma_{st}} = \frac{17244.04}{150}$$

$$= \underline{114.96 \text{ mm}^2}$$

provide 4 bars of 12mm ϕ .

$$A_{stm} = 4 \times \frac{\pi}{4} \times 12^2 = 452.33 \text{ mm}^2$$

$$\underline{452.33 > 114.96 \text{ mm}^2}$$

$$\frac{T R}{A + (m-1) A_{st}} \leq \sigma_{ct} = 1.2$$

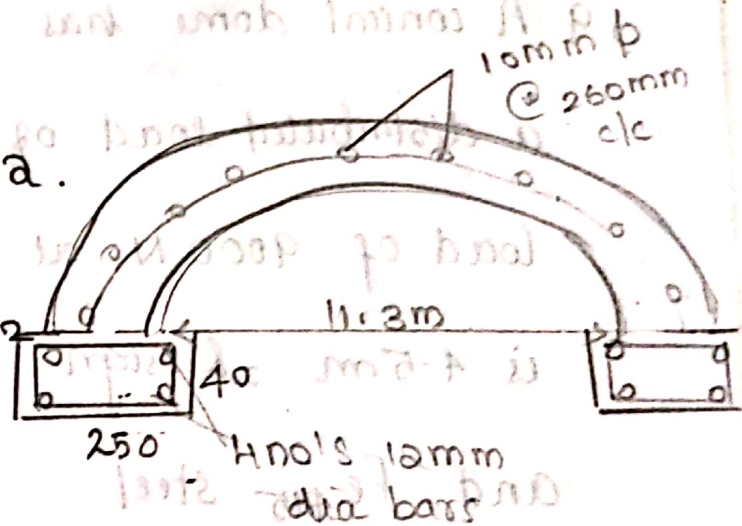
$$\frac{17244.014}{A + (14-1) 452.33}$$

$$A = \underline{8490.11 \text{ mm}^2}$$

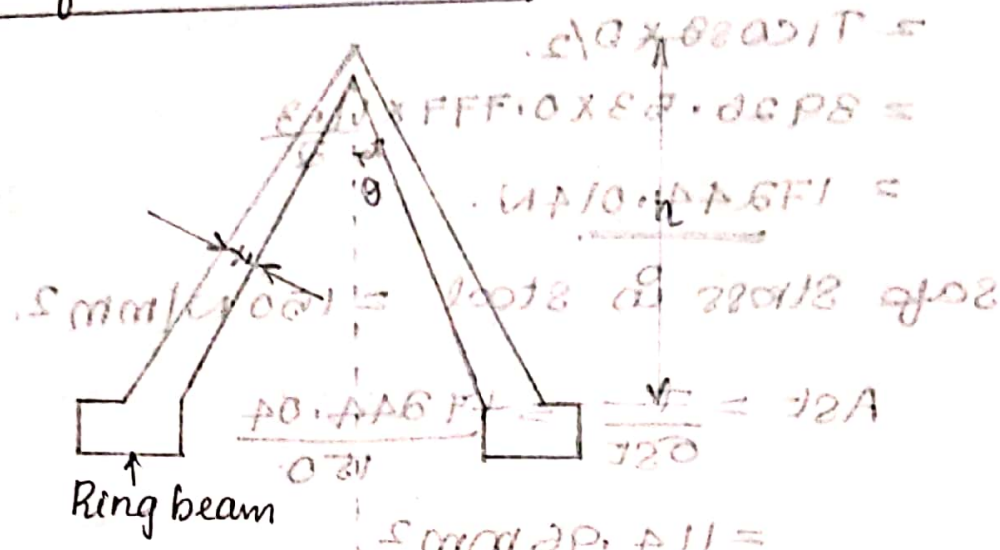
width of beam = 250mm

depth of beam = 33.96 \approx 40mm.

cls of ring beam = 250mm x 40mm.



Design of conical domes.



Meridional thrust per m run = $\frac{wh \sec^2 \theta}{2} + \frac{W \sec \theta}{2h \tan \theta}$

Hoop stress = $\frac{wh \tan^2 \theta}{t}$. (here point load is not considered) neglected

9 A conical dome has a base diameter of 9m. It carries a distributed load of 4900 N/m² and a concentrated load of 9000 N at the vertex. The height of the dome is 4.5m. Design the dome. Use M20 concrete and Fe₄₁₅ steel.

Solution

$w = 4900 \text{ N/m}^2$

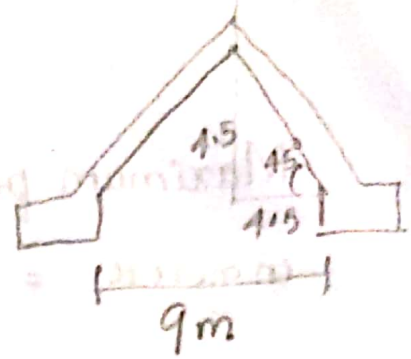
$W = 9000 \text{ N}$

Height of dome = 4.5m.

Grade of concrete = $M20$

Grade of steel = $Fe415$

Diameter of dome = $9m$



$$\sigma_{cbc} = \frac{20}{3} = 6.66 \approx 7 \text{ N/mm}^2$$

$$\sigma_{ct} = 1.2 \text{ N/mm}^2$$

$$\sigma_{st} = 150 \text{ N/mm}^2$$

$$\tan \theta = \frac{4.5}{4.5}$$

$$\theta = 45^\circ$$

Assume a thickness of $100mm$ for the dome slab.

The meridional thrust per m run at the base

↓
compressive force.

$$T = \frac{wh \sec^2 \theta}{2} + \frac{w \sec \theta}{2\pi h \tan \theta}$$

$$T = \frac{4900 \times 4.5 \sec^2 45}{2} + \frac{900 \sec 45}{2\pi \times 4.5 \tan 45}$$

$$= 22050 + 450.15$$

$$= 22500.158 \text{ N}$$

∴ Compressive stress due to meridional thrust = $\frac{T}{\text{Area}}$

* Only wdl is considered as pt load act along the center line its effect is neglected and pt load is not considered in hoop stress

$$= \frac{22500.158}{1000 \times 100}$$

$$= 0.225 \text{ N/mm}^2$$

Hoop stress = $\frac{wh \tan^2 \theta}{t \times \pi \text{ area}} = \frac{4900 \times 4.5 \times \tan^2 45}{100 \times 10^3}$

$$= 220500 \text{ N/mm}^2$$

$$= \underline{\underline{0.2205 \text{ N/mm}^2}}$$

Maximum permissible direct compressive stress of M_{20} concrete = 0.5 N/mm^2

The hoop stress and stress due to meridional thrust are very low. Hence a minimum of 0.3% steel will be provided

$$\begin{aligned} \text{Minimum steel required} &= \frac{0.3}{100} \times 1000 \times 100 \\ &= \underline{\underline{300 \text{ mm}^2}} \end{aligned}$$

Using 8mm ϕ bars,

$$\begin{aligned} \text{Spacing} &= \frac{\pi \times (8)^2 \times 1000}{4 \times 300} = \underline{\underline{167.55 \text{ mm}}} \\ &\approx \underline{\underline{165 \text{ mm}}} \end{aligned}$$

Hence provide 8mm bars @ 165mm c/c along the meridian and latitudes.

Ring beam.

Horizontal component of meridian thrust at

$$\text{the base} = T \cos \theta.$$

$$= 22500 \cos 45 = \underline{\underline{15909.9 \text{ N}}}$$

Hoop tension in the ring beam $T_R = \frac{D}{2} \times T_{\text{max}} \times \frac{D}{2}$
 $= 15909.9 \times 4.5$
 $= \underline{\underline{71594.56 \text{ N}}}$

Safe Allowing a stress of 150 N/mm^2 in the reinforcement

$$A_{st} = \frac{T_R}{\sigma_{st}} = \frac{71594.56}{150} = \underline{\underline{477.297 \text{ mm}^2}}$$

and 2 nos 12mm

Providing 2 nos 16mm diameter bars.

$$A_{st \text{ provided}} = 2 \times \frac{\pi}{4} \times (16)^2 + 2 \times \frac{\pi}{4} \times (12)^2 = \underline{\underline{628.31 \text{ mm}^2}}$$

$$A_{st \text{ req}} > A_{st \text{ pr}}$$

$$\sigma_{ct} \geq \frac{T_R}{A + (m-1)A_{st}}$$

$$1.2 \leq \frac{71594.56}{A + (1.2-1) \times 628.31}$$

$$1.2 \leq \frac{71594.56}{A + 1.2 \times 628.31}$$

$$1.2 \leq \frac{71594.56}{A + 753.972}$$

$$1.2(A + 753.972) \leq 71594.56$$

$$1.2A + 904.7664 \leq 71594.56$$

$$1.2A \leq 71594.56 - 904.7664$$

$$1.2A \leq 70689.7936$$

$$A \leq \frac{70689.7936}{1.2}$$

$$A \leq 58908.1613$$

Providing width of 250mm

∴ Depth of ring beam = $\frac{51493.99}{250}$

8mm φ rods 165mm c/c in both directions = $\frac{205.91 \text{ mm} \approx 210 \text{ mm}}$

